

ME597: AUTONOMOUS MOBILE ROBOTICS SECTION 2 – LINEAR SYSTEMS

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LINEAR ALGEBRA

- Scalar, Vector, Matrix

$$c \in \mathbb{R} \quad b = \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{bmatrix} \in \mathbb{R}^n \quad A = \begin{bmatrix} A_{11} & A_{12} & \cdots \\ A_{21} & \ddots & \\ \vdots & & A_{nm} \end{bmatrix} \in \mathbb{R}^{n \times m}$$

- Fat matrix: $n < m$, Skinny matrix: $n > m$

- Unit Vector, Identity Matrix

$$e_i = \begin{bmatrix} 0 \\ \vdots \\ 1 \\ \vdots \end{bmatrix} \quad I = \begin{bmatrix} 1 & 0 & \cdots \\ 0 & 1 & \\ \vdots & & \ddots \end{bmatrix}$$

LINEAR ALGEBRA

- Matrix Transpose

$$A^T = \begin{bmatrix} A_{11} & A_{21} & \cdots \\ A_{12} & \ddots & \\ \vdots & & \end{bmatrix}$$

- Matrix Addition

$$A+B = \begin{bmatrix} A_{11} + B_{11} & A_{12} + B_{12} & \cdots \\ A_{21} + B_{21} & \ddots & \\ \vdots & & \end{bmatrix}$$

- Matrix Multiplication

$$AB = \begin{bmatrix} \sum_i A_{1i} B_{i1} & \sum_i A_{1i} B_{i2} & \cdots \\ \sum_i A_{2i} B_{i1} & \ddots & \\ \vdots & & \end{bmatrix}$$

LINEAR ALGEBRA

- Matrix Transpose of Added Matrices

$$(A + B)^T = A^T + B^T$$

- Matrix Transpose of Multiplied Matrices

$$(AB)^T = B^T A^T$$

- Quadratic form

$$\begin{aligned}(Ax + b)^T (Ax + b) &= x^T A^T Ax + x^T A^T b + b^T Ax + b^T b \\ &= x^T A^T Ax + 2x^T A^T b + b^T b \\ &= x^T Cx + d^T x + e\end{aligned}$$

 Quadratic term

LINEAR ALGEBRA

○ Matrix Rank: $\rho(A)$

- The number of independent rows or columns
- Nonsingular = Full Rank

$$\rho(A) = \min(n, m)$$

- Singular = Not full rank

$$\rho(A) < \min(n, m)$$

- Non-empty nullspace

$$\exists x \text{ such that } Ax = 0$$

○ Matrix Inverse (square A)

$$AA^{-1} = A^{-1}A = I$$

- Nonsingular and square \Leftrightarrow Invertible

LINEAR ALGEBRA

- Matrix Trace

$$\text{tr}(A) = \sum_i A_{ii}$$

- Symmetric Matrix

$$A = A^T = \begin{bmatrix} A_{11} & A_{12} & \cdots \\ A_{12} & \ddots & \\ \vdots & & \end{bmatrix}$$

- Positive Definiteness (Semi-Definiteness)

- For a symmetric $n \times n$ matrix A , and for any x in \mathbb{R}^n

$$x^T A x > 0$$

$$(x^T A x \geq 0)$$

LINEAR ALGEBRA

- Eigenvalues and Eigenvectors of a matrix
 - For a matrix A , the vector x is an *eigenvector* of A with a corresponding *eigenvalue* λ if they satisfy the equation

$$Ax = \lambda x$$

- The eigenvalues of a diagonal matrix are its diagonal elements
- The inverse of A exists if and only if (iff) none of the eigenvalues are zero
- Positive definite A has all eigenvalues greater than zero

LINEAR ALGEBRA

- Differentiation of linear matrix equation

$$\frac{d}{dx}(Ax) = A$$

$$\frac{d}{dx}(x^T A) = A^T$$

- Differentiation of a quadratic matrix equation

$$\frac{d}{dx}(x^T Ax) = x^T A + x^T A^T$$

LINEAR ALGEBRA

○ Least Squares Solution

- If A is a skinny matrix ($n > m$), and we wish to find x for which

$$Ax = b$$

- Since A is skinny, the problem is over-constrained
 - No solution exists
- Instead, minimize the square of the error between Ax and b

$$\begin{aligned} \min_x \|Ax - b\|_2^2 \\ &= \min_x (Ax - b)^T (Ax - b) \\ &= \min_x x^T A^T Ax - 2b^T Ax + b^T b \end{aligned}$$

LINEAR ALGEBRA

- Setting the derivative to zero

$$2x^T A^T A - 2b^T A = 0$$

$$A^T A x = A^T b$$

$$x = (A^T A)^{-1} A^T b$$

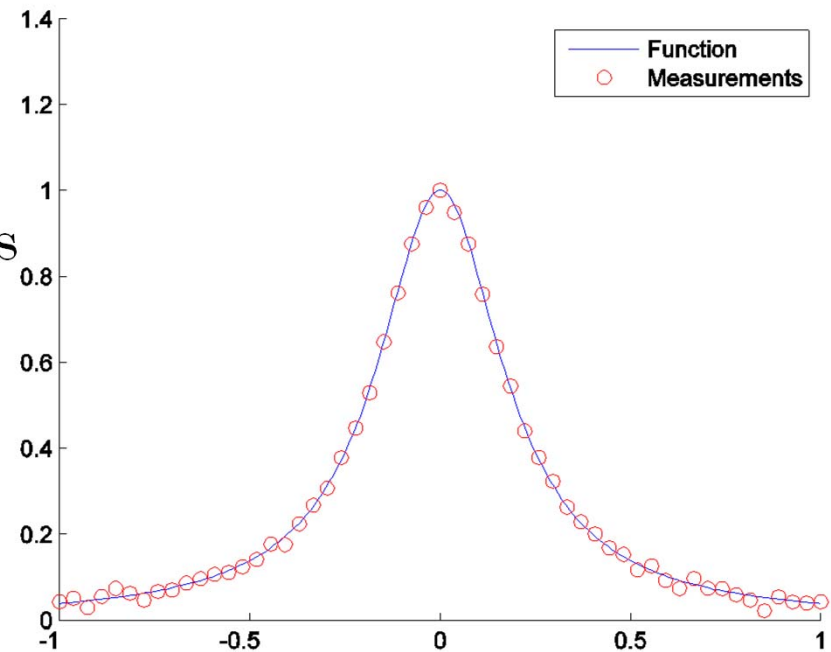
$$x = A^\dagger b$$

- Known as the pseudo-inverse
- This methodology is used over and over in the course
 - Quadratic cost minimized to find closed form solution

LINEAR ALGEBRA

- Least Squares example
 - Data fitting with polynomials
 - Given a function of interest

$$g(t) = \frac{1}{1 + 25t^2}$$



- And a set of measurements $b(t_m)$ of that function at points t_m

$$b(t_m), \quad t_m = \{-1, -0.99, \dots, 1\}$$

- Find the best polynomial fit for polynomial $f_P(t)$ of order P

$$f_P(t) = x_1 + x_2 t + \dots + x_{P+1} t^P$$

LINEAR ALGEBRA

- Least Squares example

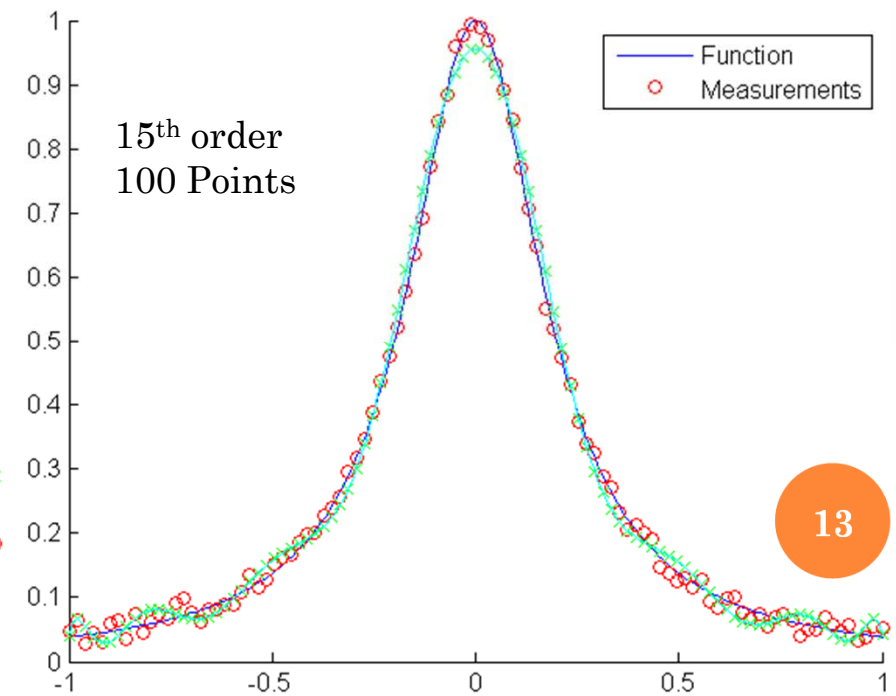
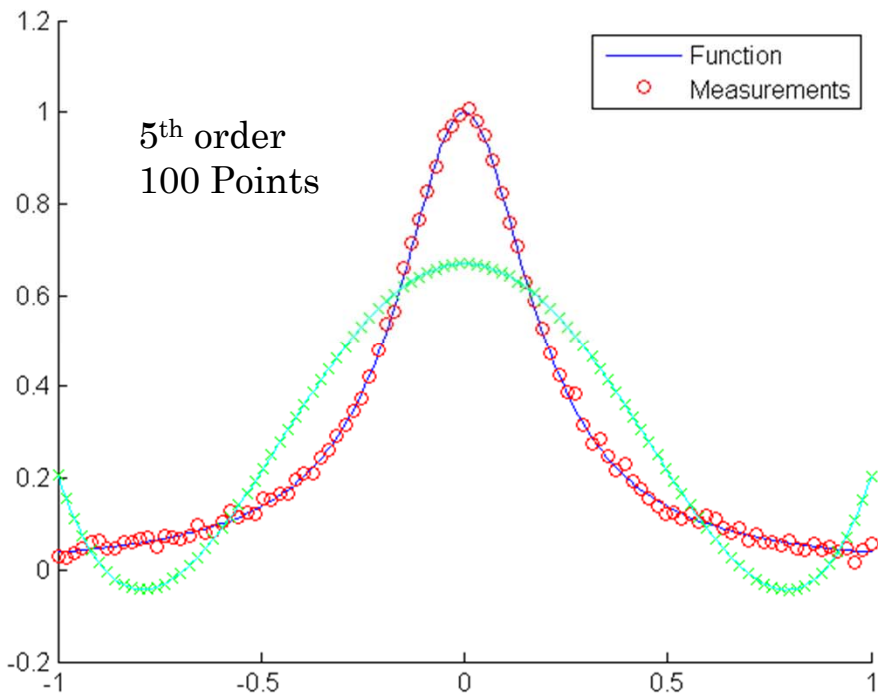
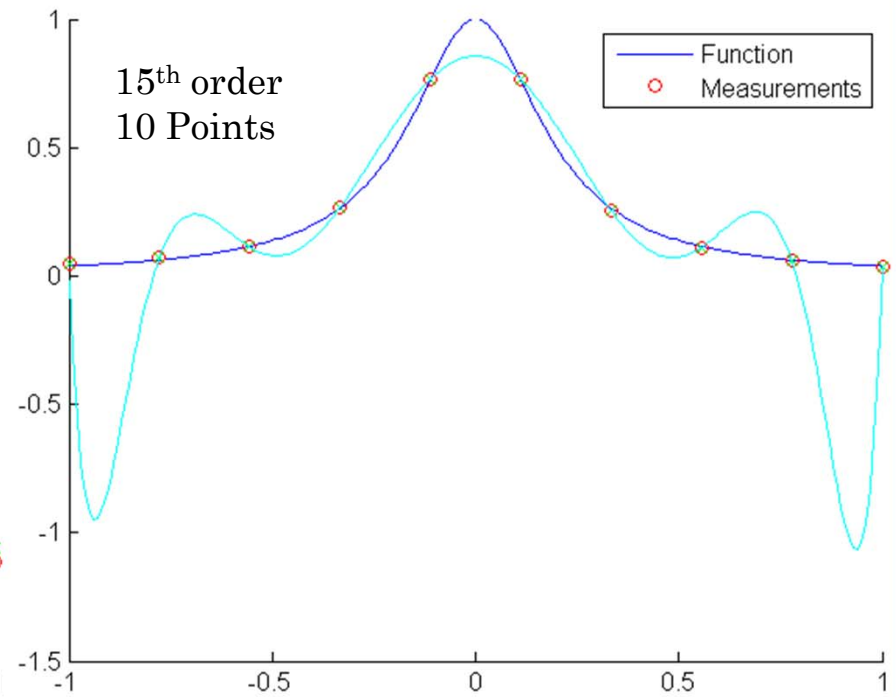
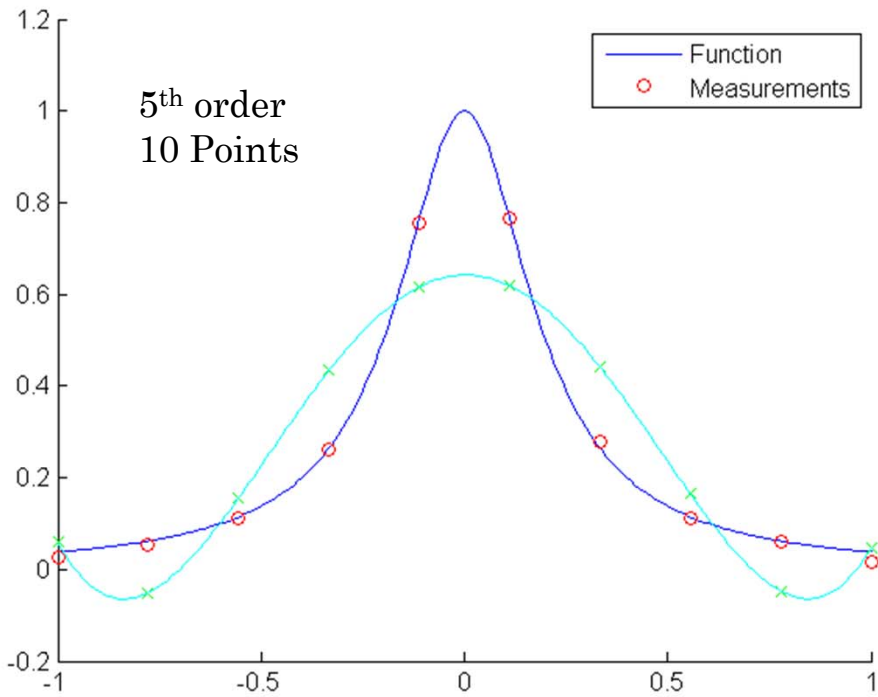
- Can formulate this as a least squares problem where we want to minimize the mean square error between polynomial prediction and measurement at each t_m :

$$\min_x \| f_P(t_m) - b(t_m) \|_2^2$$

- The polynomial can be written as

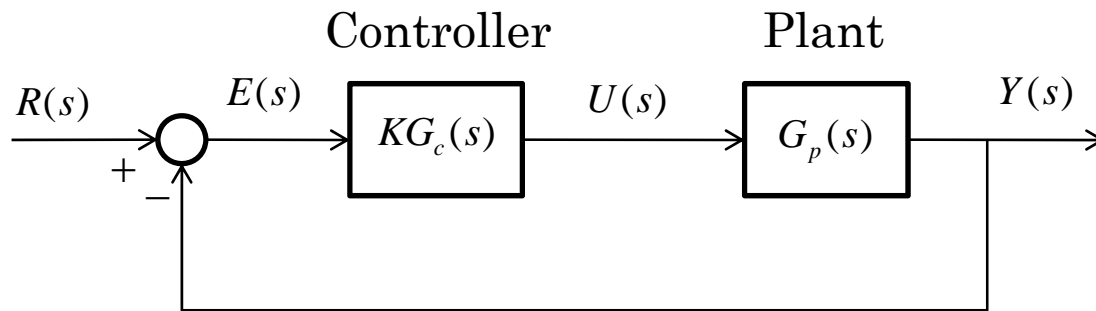
$$f_P(t_m) = A(t_m)x = x_1 + x_2 t_m + \dots + x_{P+1} t_m^P$$
$$A(t_m) = \begin{bmatrix} 1 & t_1 & t_1^2 & \dots & t_1^P \\ 1 & t_2 & t_2^2 & \dots & t_2^P \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ 1 & t_m & t_m^2 & \dots & t_m^P \end{bmatrix} \quad x = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_P \end{bmatrix}$$

- Use least squares solution method to find coefficients of f .



SISO CONTROL

- One input, one output, one transfer function between the two



Closed loop
transfer
function

$$\frac{Y(s)}{R(s)} = T(s)$$

- Model requires
 - transfer function from single input to single output
 - initial conditions to start from (usually assumed 0)
- Model hides inner workings of plant

STATE SPACE: A NEW SYSTEM MODEL

- Multi-Input-Multi-Output (MIMO) model, maintains complete plant picture
 - Matrix and vector notation, use power of linear algebra for many key results
- Definition: *The state of a system is a vector of system variables that entirely defines the system at a specific instance in time.*
 - Example: at $t=0$, initial conditions define a state vector.
 - Entire history of state variables can be discarded, only need current state and system dynamics to continue forward in time.

STANDARD FORM DYNAMICS

- Linear first order time-invariant dynamics in continuous time

- Update equation

$$\dot{x}(t) = Ax(t) + Bu(t)$$

- Measurement equation

$$y(t) = Cx(t) + Du(t)$$

- A, B matrices: state derivatives can depend on any state or input variable
- C, D matrices: output can depend on any state or input variable

STANDARD FORM DYNAMICS

- Linear first order time-invariant dynamics in discrete time

- Update equation, timesteps indexed by t

$$x_t = Ax_{t-1} + Bu_t$$

- Measurement equation

$$y_t = Cx_t + Du_t$$

- A, B matrices: state update can depend on any state or input variable
- C, D matrices: measurements can depend on any state or input variable

EXAMPLE – SPRING MASS DAMPER

- Equation of Motion

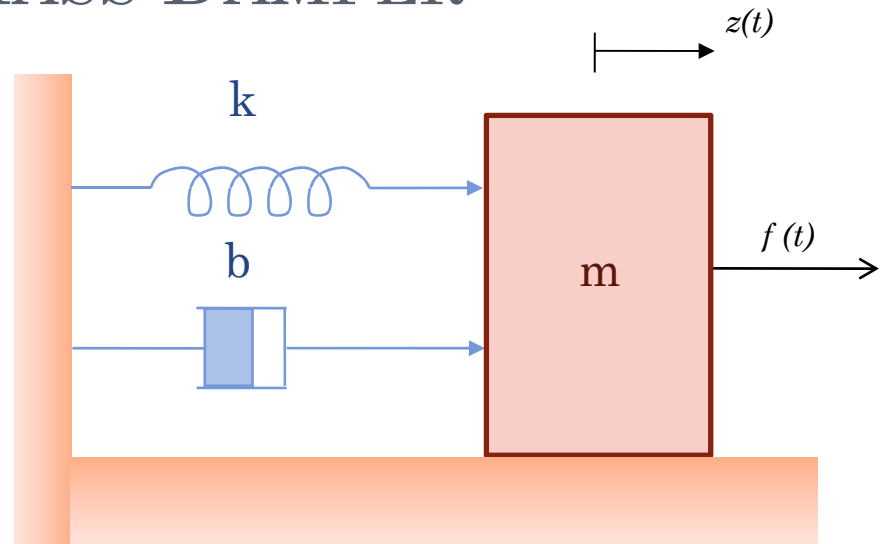
$$m\ddot{z}(t) + b\dot{z}(t) + kz(t) = f(t)$$

- Transfer function

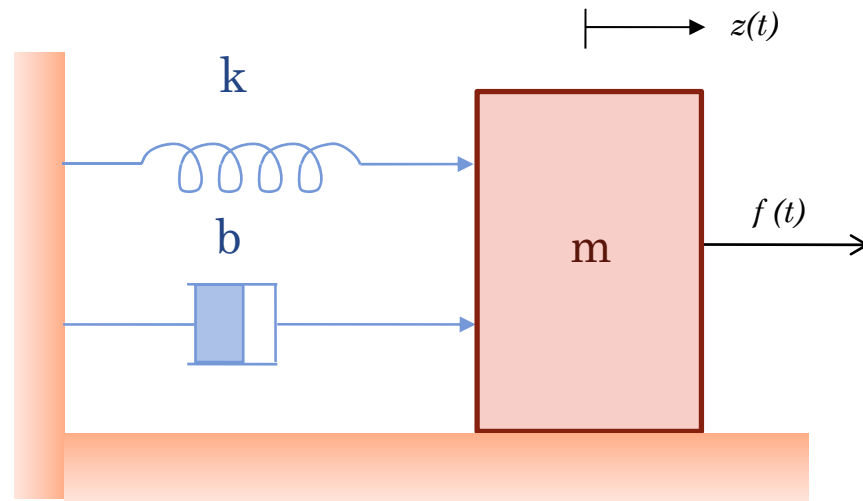
$$\frac{Z(s)}{F(s)} = \frac{1}{ms^2 + bs + k}$$

- Four variables in ODE: one input, one variable defined by ODE, two states remain.

$$x(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} z(t) \\ \dot{z}(t) \end{bmatrix}$$



EXAMPLE CONT'D



- Motion Model

$$\begin{bmatrix} \dot{z}(t) \\ \ddot{z}(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix} \begin{bmatrix} z(t) \\ \dot{z}(t) \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix} f(t)$$

$$\dot{x}(t) = Ax(t) + Bu(t)$$

- Measurement model: position and velocity sensors

$$\begin{bmatrix} y_1(t) \\ y_2(t) \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} z(t) \\ \dot{z}(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \end{bmatrix} f(t)$$

$$y = Cx(t) + Du(t)$$

IN TRANSFER FUNCTION FORM

- Take Laplace transform of update equation

$$\frac{dx(t)}{dt} = Ax(t) + Bu(t) \quad \longrightarrow \quad sX(s) - x(0) = AX(s) + BU(s)$$

- Solve for $X(s)$, with $x(0)=0$

$$(sI - A)X(s) = BU(s)$$

$$X(s) = (sI - A)^{-1}BU(s)$$

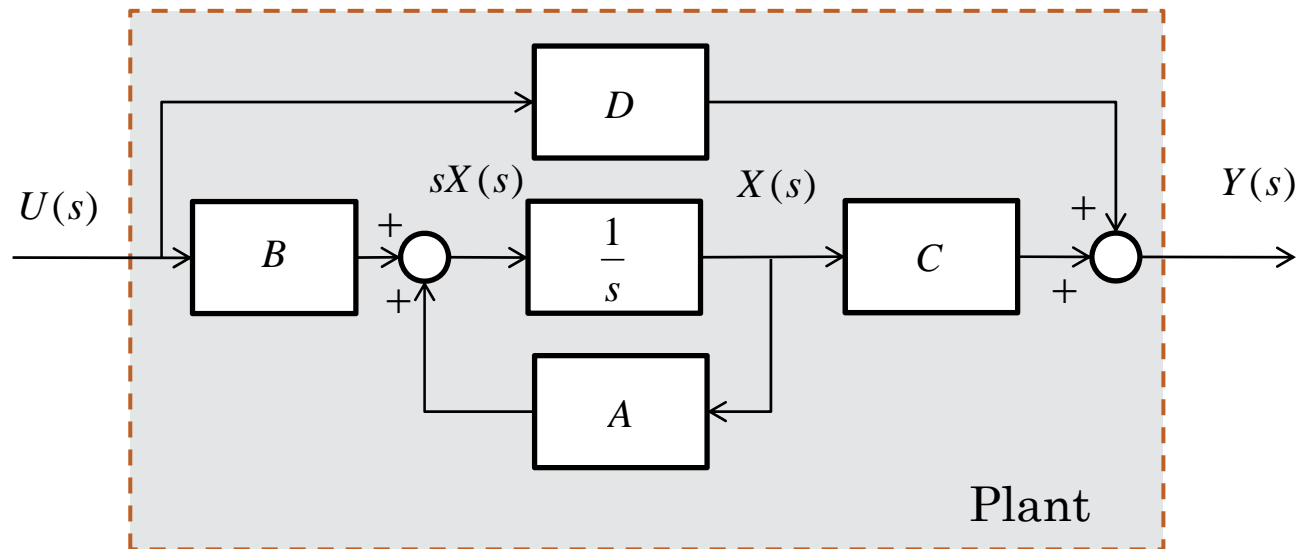
- Combine with measurement model

$$Y(s) = CX(s) + DU(s)$$

$$\frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + D$$

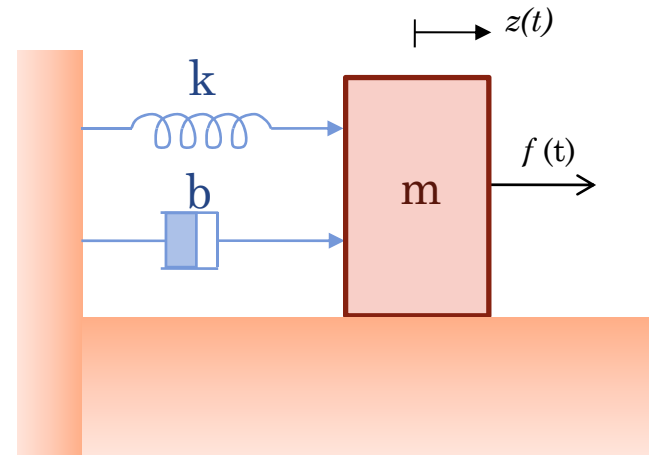
BLOCK DIAGRAM

- Continuous LTI State space model as a block diagram (Laplace Domain)



EXAMPLE: FIND TFS

$$A = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}, B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}, C = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, D = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$



$$\frac{Y(s)}{U(s)} = C(sI - A)^{-1}B$$

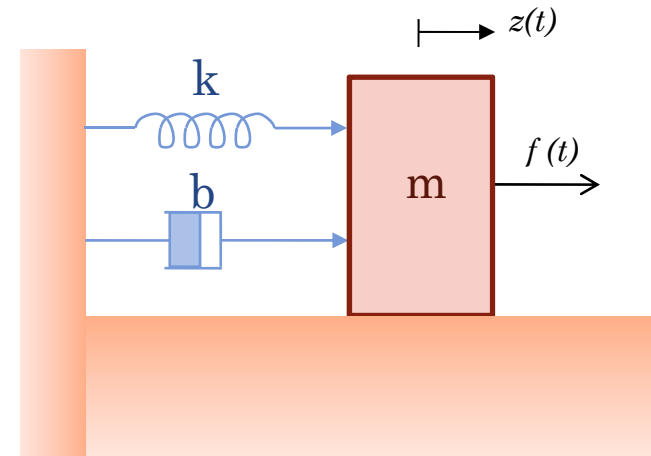
$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \left(\begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{b}{m} \end{bmatrix} \right)^{-1} \begin{bmatrix} 0 \\ 1 \\ m \end{bmatrix}$$

$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \left(\begin{bmatrix} s & -1 \\ \frac{k}{m} & s + \frac{b}{m} \end{bmatrix} \right)^{-1} \begin{bmatrix} 0 \\ 1 \\ m \end{bmatrix}$$

EXAMPLE: FIND TFS

$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \frac{1}{\det(sI - A)} \begin{pmatrix} s + \frac{b}{m} & 1 \\ -\frac{k}{m} & s \end{pmatrix} \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix}$$

$$\frac{Y(s)}{U(s)} = \begin{bmatrix} \frac{1}{\det(sI - A)} \\ \frac{s}{\det(sI - A)} \end{bmatrix} = \begin{bmatrix} \frac{1}{m} \\ s^2 + \frac{b}{m}s + \frac{k}{m} \\ \frac{s}{m} \\ s^2 + \frac{b}{m}s + \frac{k}{m} \end{bmatrix}$$



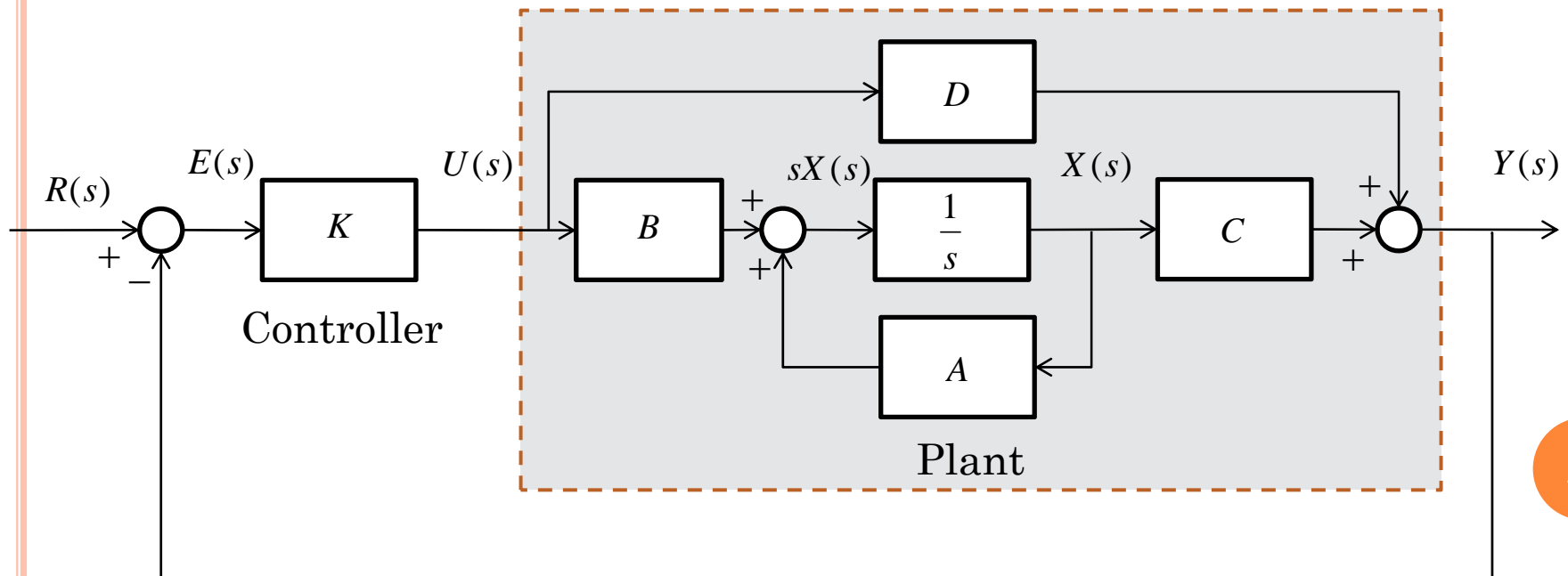
- So roots of $\det(sI-A)$ determine poles of open loop system
 - Well known equation in linear algebra: eigenvalues/eigenvectors
 - Open loop poles are eigenvalues of A
 - Holds for all sizes of A , not just 2×2

STATE FEEDBACK CONTROL

- If $C = I$ and $D = 0$, full state feedback
 - More than one signal, in fact everything we could possibly need

$$u(t) = -Kx(t)$$

- Assume $R(s) = 0$ (regulator)



STATE FEEDBACK

- Closed loop transfer function

$$\frac{X(s)}{R(s)} = (sI - A + BK)^{-1}$$

- Now, eigenvalues of $A-BK$ are poles of closed loop system
- In fact, since there is one K for every eigenvalue, we can place the closed loop poles anywhere we'd like.

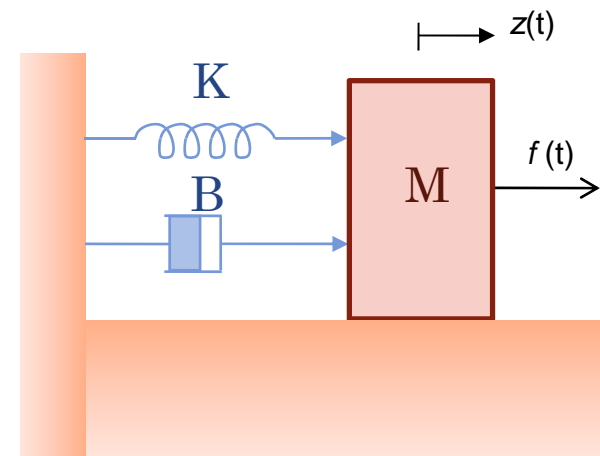
EXAMPLE: POLE PLACEMENT

- Lets place closed loop poles at
- Note: $BK = \begin{bmatrix} 0 \\ \frac{1}{m} \end{bmatrix} [K_1 \quad K_2] = \begin{bmatrix} 0 & 0 \\ \frac{K_1}{m} & \frac{K_2}{m} \end{bmatrix}$
- Match coefficients of polynomials
 - Desired = actual

$$s^2 + 10s + 50 = \det \left(\begin{bmatrix} s & -1 \\ \frac{k}{m} + \frac{K_1}{m} & s + \frac{b}{m} + \frac{K_2}{m} \end{bmatrix} \right)$$

$$= s^2 + \left(\frac{K_2}{m} + \frac{b}{m} \right) s + \left(\frac{K_1}{m} + \frac{k}{m} \right)$$

$$s = -5 \pm 5j$$

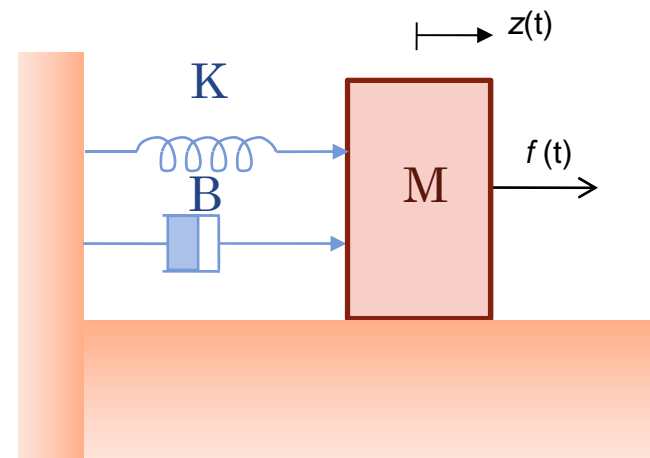


EXAMPLE: CONTROLLER

- What is full state feedback?

$$u(t) = K_1 z(t) + K_2 \dot{z}(t)$$

- PD control
- To add integral control, add an integrator state



$$x(t) = \begin{bmatrix} \int z dt \\ z \\ \dot{z} \end{bmatrix}, \quad A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0 & -\frac{k}{m} & -\frac{b}{m} \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 0 \\ \frac{1}{m} \end{bmatrix}$$

CONTROLLABILITY

- Can I get there from here?
 - A system is controllable if for any set of initial and final states, $x(0)$ and $x(T)$, there exists a control input sequence, $u(0)$ to $u(T)$, to get from $x(0)$ to $x(T)$.
 - Can be checked easily: The following matrix must be full rank

$$\text{rank}\left(\begin{bmatrix} B & AB & A^2B & \cdots & A^{n-1}B \end{bmatrix}\right) = n$$

OBSERVABILITY

- Can I see there from here?
 - Given any sequence of states $x(0)$ to $x(T)$, inputs $u(0)$ to $u(T)$ and outputs $y(0)$ to $y(T)$, a system is observable if the state can be uniquely determined from the outputs alone.
- Again, an easy check on the observability matrix determines if a system is observable

$$\text{rank} \begin{pmatrix} \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{bmatrix} \end{pmatrix} = n$$

OPTIMAL CONTROL

- Since we can place poles anywhere, can change objective of control design
- Minimize quadratic errors in states and quadratic use of inputs

$$\min_{x,u} \int_0^t x^T(\tau)Qx(\tau) + u^T(\tau)Ru(\tau)d\tau$$

- Penalize big deviations more heavily than small ones
- Quadratic cost and linear dynamics result in a time invariant control law, another way to set the gains for state feedback control

OPTIMAL ESTIMATION

- The second half of the model describes the relationship between the state and the measured outputs.
 - Any sensor dynamics must be included in the state
- In reality, both disturbances and noise will exist

$$\dot{x}(t) = Ax(t) + Bu(t) + w(t)$$

$$y(t) = Cx(t) + Du(t) + v(t)$$

- Assume w, v are Gaussian white noise with covariance Q, R
- Assume $u(t)$ is known exactly
- Formulate minimum mean squared error estimation problem, results in Kalman filter

STATE SPACE MODEL

